General Description

The LTA181 series of bidirectional zero-drift current sense amplifier is designed for cost optimized solution, which can sense drops across shunts at common-mode voltages from –0.2 V to 30 V, independent of the supply voltage. Unidirectional operation allows the LTA181 series to measure currents through a resistive shunt in one direction, while bidirectional operation allows the device to measure currents through a resistive shunt in two directions. The low offset of the zero-drift architecture enables current sensing with maximum drops across the shunt as low as 10mV full-scale.

The LTA181 series operates from a single +2.7 V to +5.5 V power supply, drawing a maximum of 180 µA of supply current. The device is specified from –40℃ to +105℃, and offered in SOT23-6L and SC70-6L packages.

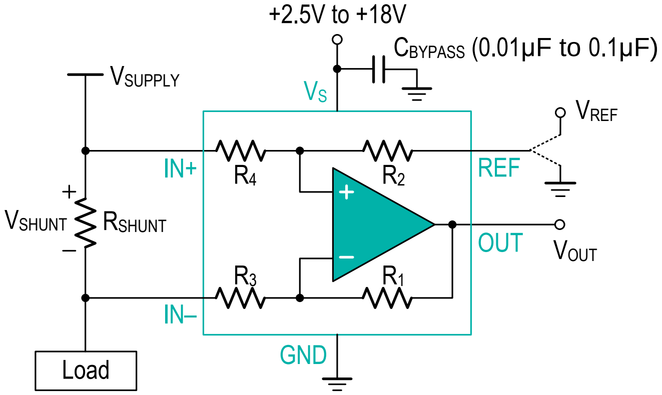
Features and Benefits

- Wide common-mode range: -0.2 V to 30 V
- Maximum ±150 µV Offset voltage at V_{cm} = 0V
- Accuracy
  - Maximum ±1 % Gain Error
  - Maximum 1.5 µV/℃ Offset Drift
  - Maximum 20 ppm/℃ Gain Drift
- Choice of Gains:
  - LTA181A1: 20 V/V
  - LTA181A2: 50 V/V
  - LTA181A3: 100 V/V
  - LTA181A4: 200 V/V
- Quiescent Current: Maximum 180 µA
- Package: SOT23-6L, SC70-6L

Applications

- Power Management
- Battery Chargers
- Electrical Cigarette
- Smart Phones and Tablets
- Notebook Computers
- Telecom Equipments
- Welding Equipments

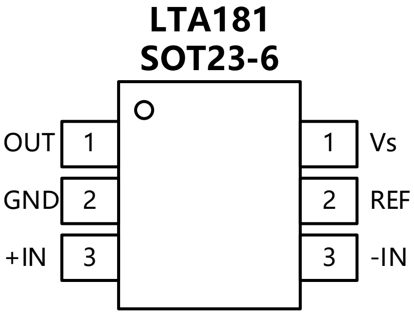
Block Diagram and Pin Configuration (Top View)

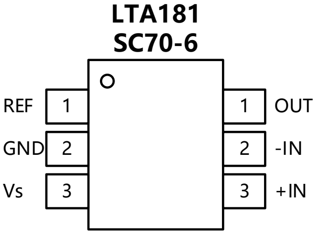


High-side Sensing Application

LINEARIN

Package Information





Pin Description

Symbol	Description
IN−	Inverting input of the amplifier.
IN+	Non-inverting input of the amplifier.
OUT	Amplifier output. The voltage range extends to within millivolt of each supply rail.
REF	Reference voltage
V_S	Positive power supply. Typically, the voltage is from +2.7 V to +5.5 V. A bypass capacitor of 0.1µF as close to the part as possible should be used between power supply pin and ground pin.
GND	Negative power supply.

Ordering Information

Orderable Type Number	Package Name	Package Quantity	Eco Class[1]	Marking Code
LTA181A1XT6/R6	SOT23-6L	3 000	Green (RoHS & no Sb/Br)	8R1
LTA181A1XC6/R6	SC70-6L	3 000	Green (RoHS & no Sb/Br)	8R1
LTA181A2XT6/R6	SOT23-6L	3 000	Green (RoHS & no Sb/Br)	8R2
LTA181A2XC6/R6	SC70-6L	3 000	Green (RoHS & no Sb/Br)	8R2
LTA181A3XT6/R6	SOT23-6L	3 000	Green (RoHS & no Sb/Br)	8R3
LTA181A3XC6/R6	SC70-6L	3 000	Green (RoHS & no Sb/Br)	8R3
LTA181A4XT6/R6	SOT23-6L	3 000	Green (RoHS & no Sb/Br)	8R4
LTA181A4XC6/R6	SC70-6L	3 000	Green (RoHS & no Sb/Br)	8R4

(1) Eco Class - The planned eco-friendly classification: Pb-Free (RoHS) or Green (RoHS & Halogen Free).
(2) Please contact to your Linearin representative for the latest availability information and product content details.

Limiting Value

In accordance with the Absolute Maximum Rating System (IEC 60134).

Parameter	Absolute Maximum Rating
Supply Voltage, V_S to GND	+6 V
Analog Input (IN+, IN–), Differential (V_{IN+} – V_{IN-})	–30 V to +30 V
Analog Input (IN+, IN–), Common-Mode	(GND – 0.3 V) to +30 V
REF Input	(GND – 0.3 V) to (V_+ + 0.3 V)
Output	(GND – 0.3 V) to (V_+ + 0.3 V)
Input Current Into All Pins	5 mA
Storage Temperature Range	–65℃ to +150℃
Junction Temperature	150℃
Lead Temperature Range (Soldering 10 sec)	260℃

Thermal Information

Thermal Metric		Package		Unit
θ_{JA}	Package Thermal Resistance	SOT23-6L	250	℃/W
		SC70-6L		

ESD Rating

Parameter	Item	Value	Unit
Electrostatic Discharge Voltage	Human body model (HBM), per MIL-STD-883J / Method 3015.9 (1)	TBH	V
	Charged device model (CDM), per ESDA/JEDEC JS-002-2014 (2)	TBH	
	Machine model (MM), per JESD22-A115C	TBH	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

Electrical Characteristics

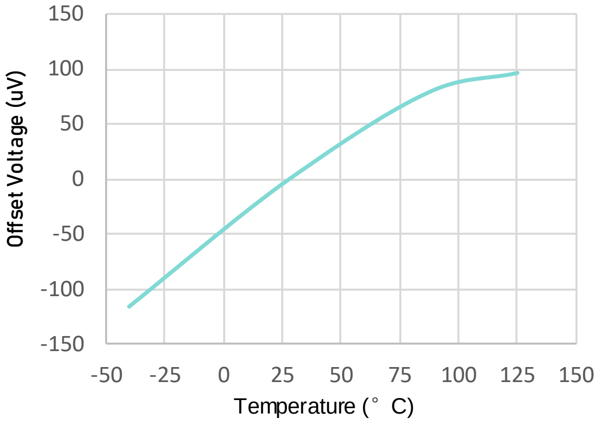
T_A = +25℃, V_S = +5.0V, V_{IN+} = 12V, V_{SENSE} = V_{IN+} − V_{IN-}, and V_{REF} = V_S/2, unless otherwise noted.
Boldface limits apply over the specified temperature range, T_A = −40 to +105 ℃.

Symbol	Parameter	Conditions	Min.	Typ.	Max.	Unit
INPUT CHARACTERISTICS						
V_{OS}	RTI, offset voltage	V_{SENSE} = 0mV		±25	±150	µV
V_{OS} TC	Offset voltage drift	*over Temperature, V_{SENSE} = 0 mV*		*1*	*1.5*	*µV/℃*
I_B	Input bias current	V_{SENSE} = 0mV		25		µA
I_{OS}	Input offset current	V_{SENSE} = 0mV		±0.4		µA
V_{CM}	Common-mode input voltage range		-0.2		30	V
CMRR	RTI, Common-mode rejection ratio	V_{IN+} = 0 V to +26V, V_{SENSE} = 0mV	90	105		dB
OUTPUT CHARACTERISTICS						
G	Gain	LTA181A1		20		V/V
		LTA181A2		50		
		LTA181A3		100		
		LTA181A4		200		
E_G	Gain error	***V_{sense} = -40mV to 40mV***		***0.5***	*1*	***%***
E_G TC	Gain error drift	*over Temperature*		*15*		***ppm/℃***
	Nonlinearity Error	V_{OUT} = 0.5 V to V_s-0.5 V		±0.01		%
C_L	Maximum Capacitive Load	No sustained oscillation		1		nF
V_{OH}	Swing to V_S rail	R_L = 10kΩ to GND		Vs-60		mV
V_{OL}	Swing to GND			V_{GND}+3		
DYNAMIC PERFORMANCE						
BW	Bandwidth	LTA181A1, C_{LOAD} = 10pF		TBH		kHz
		LTA181A2, C_{LOAD} = 10pF		130		
		LTA181A3, C_{LOAD} = 10pF		TBH		
		LTA181A4, C_{LOAD} = 10pF		TBH		
SR	Slew rate			1.2		V/µs
NOISE PERFORMANCE						
e_n	Voltage noise density	Referred-to-input		40		nV/√Hz
POWER SUPPLY						
V_S	Operating supply voltage			2.7	5.5	V
PSR	Input vs power supply	V_S = +2.5V to +5.5V, V_{IN+} = +12V, V_{SENSE} = 0mV		±3	±10	µV/V
I_Q	Quiescent current	V_{SENSE} = 0mV		130	180	µA
	over Temperature				*290*	
THERMAL CHARACTERISTICS						
T_A	Operating temperature		-40		+125	℃

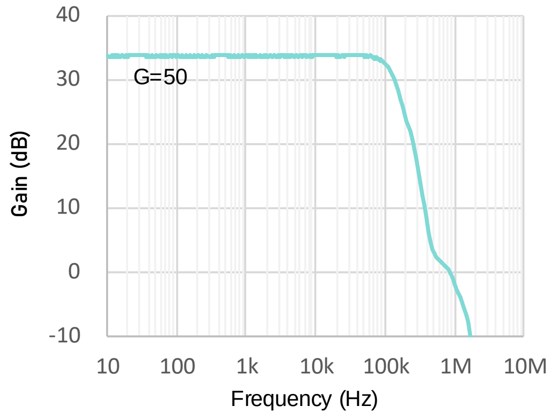
LINEARIN

Typical Performance Characteristics

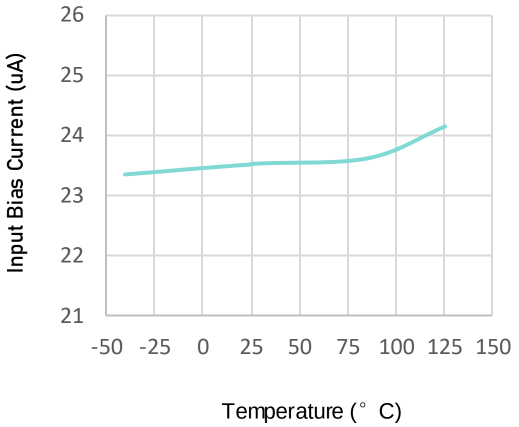
At T_A = +25℃, V_S = +5.0V, V_{IN+} = 12V, and V_{REF} = V_S/2, unless otherwise noted.



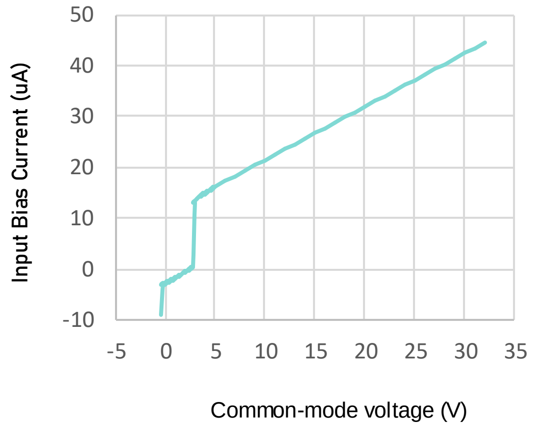
Offset Voltage vs. Temperature



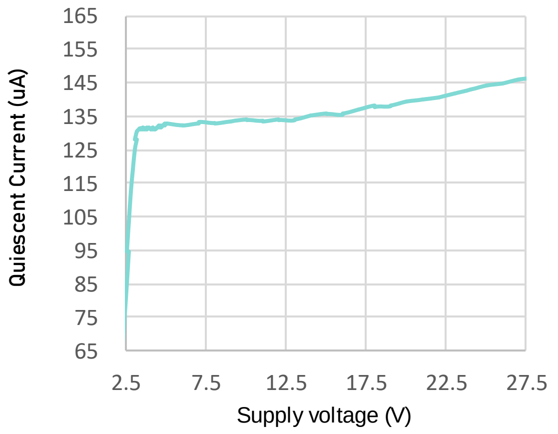
Gain vs. Frequency



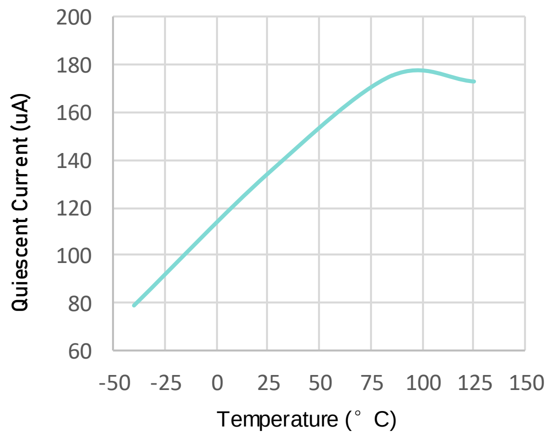
Input Bias Current vs. Temperature



Input Bias Current vs. Common-mode voltage with power supply=5V



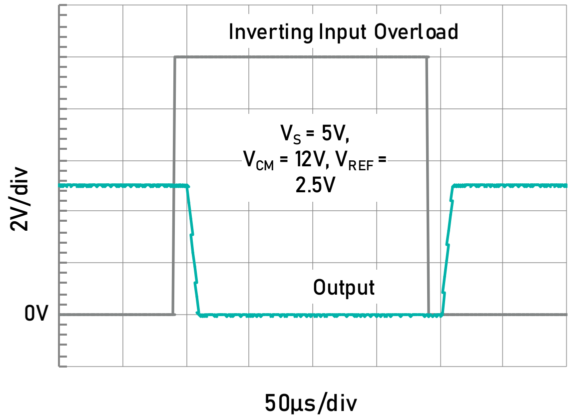
Quiescent Current vs. Supply Voltage



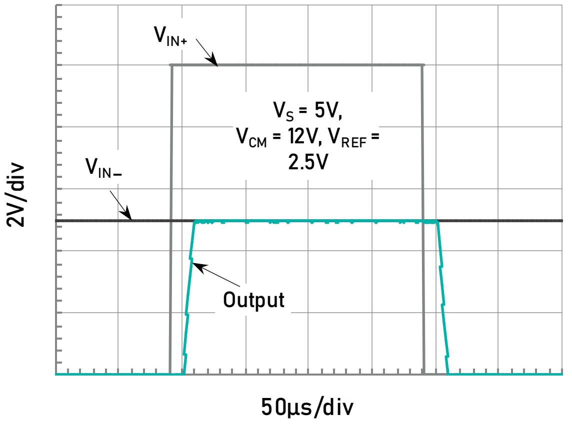
Quiescent Current vs. Temperature

Typical Performance Characteristics (continued)

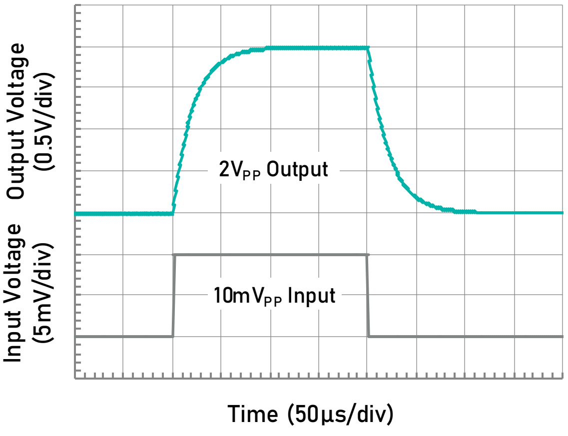
At T_A = +25°C, V_S = +5.0V, V_{IN+} = 12V, and V_{REF} = V_S/2, unless otherwise noted.



Inverting Differential Input Overload



Noninverting Differential Input Overload



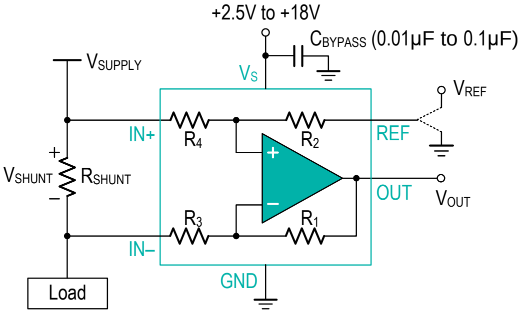
Step Response ($10mV_{PP}$ Input Step)

Application Notes

BASIC CONNECTIONS

Figure 1 shows the basic connections for the LTA181. The input pins, IN+ and IN–, should be connected as closely as possible to the shunt resistor to minimize any resistance in series with the shunt resistance.

Power-supply bypass capacitors are required for stability. Applications with noisy or high-impedance power supplies may require additional decoupling capacitors to reject power-supply noise. Connect bypass capacitors close to the device pins.



High-side Sensing Application

Figure 1. Typical Application

POWER SUPPLY

The input circuitry of the LTA181 can accurately measure beyond its power-supply voltage, V_S. For example, the V_S power supply can be 5V, whereas the load power-supply voltage can be as high as +18V. However, the output voltage range of the OUT terminal is limited by the voltages on the power-supply pin. Note also that the LTA181 can withstand the full –xxx V to +xxx V range in the input pins, regardless of whether the device has power applied or not.

SELECTING R_S

The zero-drift offset performance of the LTA181 offers several benefits. Most often, the primary advantage of the low offset characteristic enables lower full-scale drops across the shunt. For example, non-zero-drift current sense amplifiers typically require a full-scale range of 100mV.

The LTA181 of current sense amplifier gives equivalent accuracy at a full-scale range on the order of 10mV. This accuracy reduces shunt dissipation by an order of magnitude with many additional benefits.

Alternatively, there are applications that must measure current over a wide dynamic range that can take advantage of the low offset on the low end of the measurement. Most often, these applications can use the lower gain of 100 to accommodate larger shunt drops on the upper end of the scale.

UNIDIRECTIONAL OPERATION

Unidirectional operation allows the LTA181 to measure currents through a resistive shunt in one direction. The most frequent case of unidirectional operation sets the output at ground by connecting the REF pin to ground. In unidirectional applications where the highest possible accuracy is desirable at very low inputs, bias the REF pin to a convenient value above 50mV to get the device output swing into the linear range for zero inputs.

A less frequent case of unipolar output biasing is to bias the output by connecting the REF pin to the supply; in this case, the quiescent output for zero input is at quiescent supply. This configuration would only respond to negative currents (inverted voltage polarity at the device input).

BIDIRECTIONAL OPERATION

Bidirectional operation allows the LTA181 to measure currents through a resistive shunt in two directions. In this case, the output can be set anywhere within the limits of what the reference inputs allow (that is, between 0V to V+). Typically, it is set at half-scale for equal range in both directions. In some cases, however, it is set at a voltage other than half-scale when the bidirectional current is nonsymmetrical.

The quiescent output voltage is set by applying voltage to the reference input. Under zero differential input conditions the output assumes the same voltage that is applied to the reference input.

INPUT FILTERING

An obvious and straightforward filtering location is at the device output. However, this location negates the advantage of the low output impedance of the internal buffer. The only other filtering option is at the device input pins. This location, though, does require consideration of the $\pm$30% tolerance of the internal resistances. Figure 2 shows a filter placed at the inputs pins.

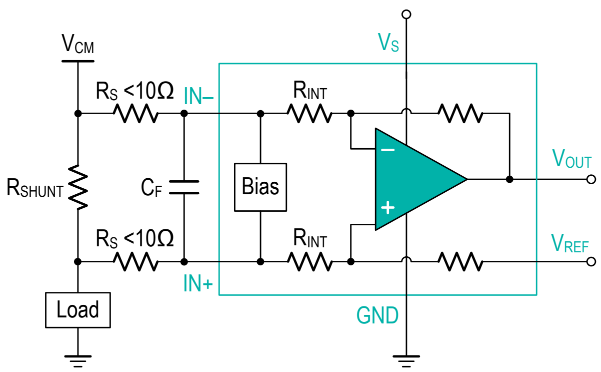


Figure 2. Filter at Input Pins

The addition of external series resistance, however, creates an additional error in the measurement so the value of these series resistors should be kept to 10Ω or less if possible to reduce impact to accuracy. The internal bias network shown in Figure 2 present at the input pins creates a mismatch in input bias currents when a differential voltage is applied between the input pins. If additional external series filter resistors are added to the circuit, the mismatch in bias currents results in a mismatch of voltage drops across the filter resistors. This mismatch creates a differential error voltage that subtracts from the voltage developed at the shunt resistor. This error results in a voltage at the device input pins that is different than the voltage developed across the shunt resistor. Without the additional series resistance, the mismatch in input bias currents has little effect on device operation. The amount of error these external filter resistor add to the measurement can be calculated using Equation 2 where the gain error factor is calculated using Equation 1.

The amount of variance in the differential voltage present at the device input relative to the voltage developed at the

Application Notes (continued)

shunt resistor is based both on the external series resistance value as well as the internal input resistors, R_{INT} as shown in Figure 2. The reduction of the shunt voltage reaching the device input pins appears as a gain error when comparing the output voltage relative to the voltage across the shunt resistor. A factor can be calculated to determine the amount of gain error that is introduced by the addition of external series resistance. The equation used to calculate the expected deviation from the shunt voltage to what is seen at the device input pins is given in Equation 1:

$$\text{Gain Error Factor} = \frac{1250 \times R_{INT}}{1250 \times R_S + 1250 \times R_{INT} + R_S \times R_{INT}}$$

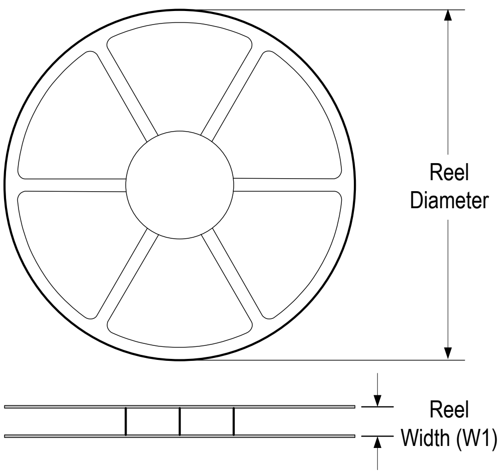
where:
R_{INT} is the internal input resistor (R3 and R4, 10kΩ), and
R_S is the external series resistance.
The gain error that can be expected from the addition of the external series resistors can then be calculated based on Equation 2:

$$\text{Gain Error (\%)} = 100 - (100 \times \text{Gain Error Factor})$$

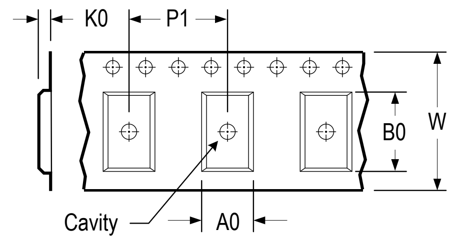
For LTA181, a series resistance of 10Ω results in a gain error factor of 0.991. The corresponding gain error is then calculated using Equation 2, resulting in a gain error of approximately 0.89% solely because of the external 10Ω series resistors.

Tape and Reel Information

REEL DIMENSIONS

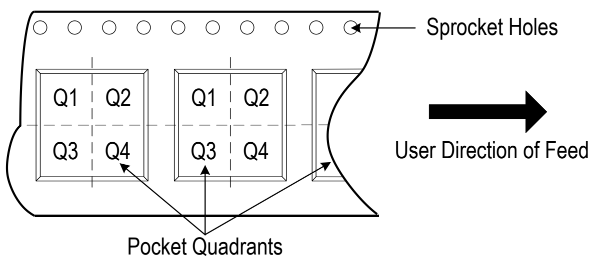


TAPE DIMENSIONS



A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIETATION IN TAPE

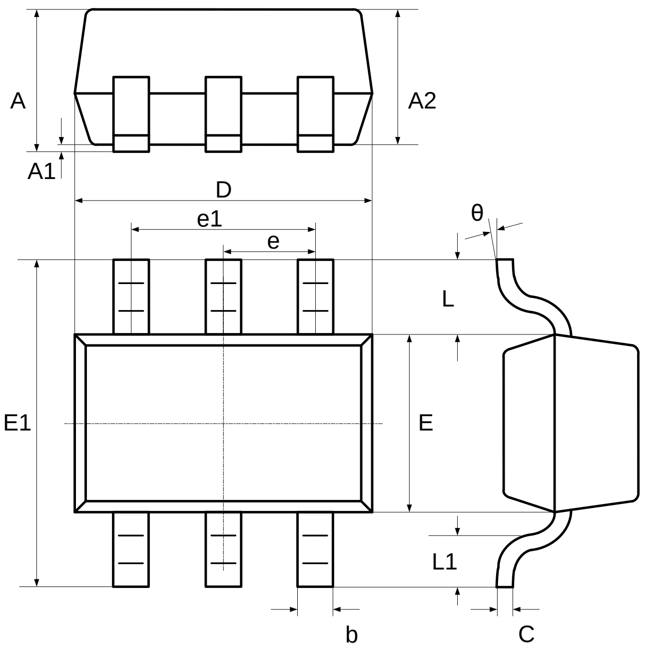


* All dimensions are nominal

Device	Package Type	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin 1 Quadrant
LTA181A1XC6/R6	SC70	6	3 000	178.0	10.0	4.0	3.5	1.5	4.0	8.0	Q3
LTA181A2XC6/R6	SC70	6	3 000	178.0	10.0	4.0	3.5	1.5	4.0	8.0	Q3
LTA181A3XC6/R6	SC70	6	3 000	178.0	10.0	4.0	3.5	1.5	4.0	8.0	Q3
LTA181A4XC6/R6	SC70	6	3 000	178.0	10.0	4.0	3.5	1.5	4.0	8.0	Q3
LTA181A1XT6/R6	SOT23	6	3 000	178.0	9.0	3.3	3.2	1.5	4.0	8.0	Q3
LTA181A2XT6/R6	SOT23	6	3 000	178.0	9.0	3.3	3.2	1.5	4.0	8.0	Q3
LTA181A3XT6/R6	SOT23	6	3 000	178.0	9.0	3.3	3.2	1.5	4.0	8.0	Q3
LTA181A4XT6/R6	SOT23	6	3 000	178.0	9.0	3.3	3.2	1.5	4.0	8.0	Q3

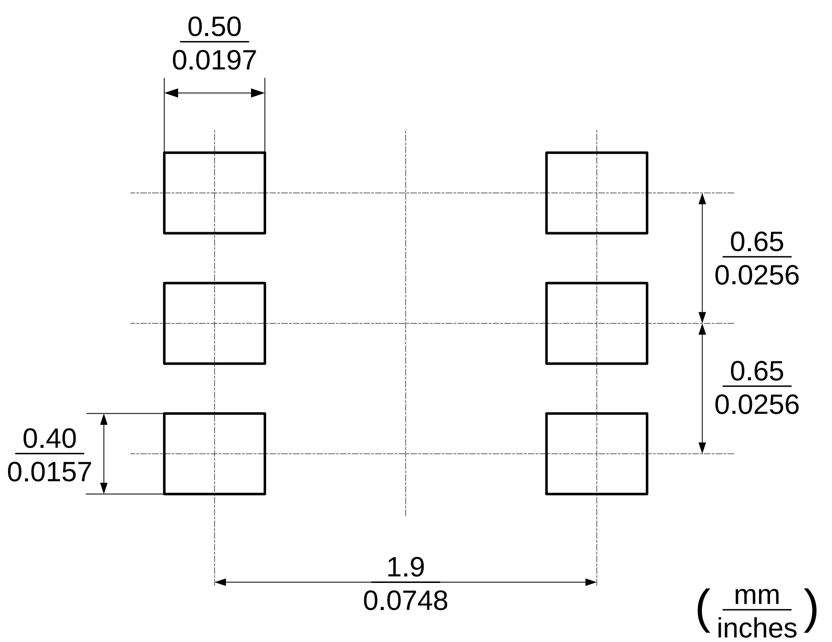
Package Outlines

DIMENSIONS, SC70-6L(SOT363)



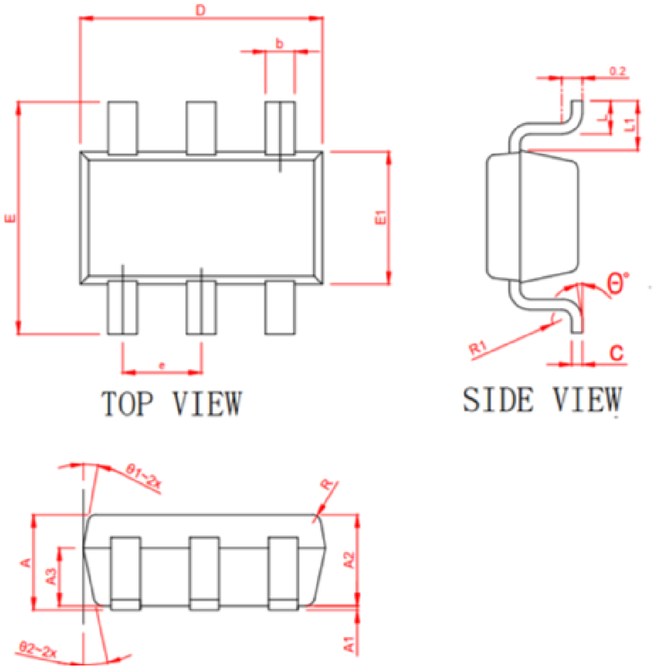
Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	0.80	1.10	0.031	0.043
A1	0.00	0.10	0.000	0.004
A2	0.80	1.00	0.031	0.039
b	0.15	0.30	0.006	0.012
C	0.10	0.25	0.004	0.010
D	1.85	2.20	0.073	0.087
E	1.15	1.35	0.045	0.053
E1	1.80	2.40	0.071	0.094
e	0.65 typ.		0.026 typ.	
e1	1.20	1.40	0.047	0.055
L	0.42 ref.		0.017 ref.	
L1	0.10	0.45	0.004	0.018
θ	0°	8°	0°	8°

RECOMMENDED SOLDERING FOOTPRINT, SC70-6L (SOT363)



Package Outlines

DIMENSIONS, SOT23-6L



SYMBOL	MILLIMETER		
	MIN	NOM	MAX
A	1.10	1.15	1.25
* A1	0.02	0.06	0.10
* A2	1.05	1.10	1.15
A3	0.60	0.65	0.70
* b	0.32	0.35	0.48
* c	0.152REF		
* D	2.87	2.92	2.97
* E	2.60	2.80	3.00
* E1	1.55	1.60	1.65
* e	0.95BSC		
* L	0.35	0.45	0.55
L1	0.60 REF		
R	0.10 REF		
R1	0.12 REF		
* θ	0°	3°	6°
θ1	7°BSC		
θ2	10°BSC		

IMPORTANT NOTICE

Linearin is a global fabless semiconductor company specializing in advanced high-performance high-quality analog/mixed-signal IC products and sensor solutions. The company is devoted to the innovation of high performance, analog-intensive sensor front-end products and modular sensor solutions, applied in multi-market of medical & wearable devices, smart home, sensing of IoT, and intelligent industrial & smart factory (industrial 4.0). Linearin's product families include widely-used standard catalog products, solution-based application specific standard products (ASSPs) and sensor modules that help customers achieve faster time-to-market products. Go to http://www.linearin.com for a complete list of Linearin product families.

For additional product information, or full datasheet, please contact with the Linearin's Sales Department or Representatives.